



# 2021-01-0420 Electrified Deceleration Cylinder Cutoff Engine Control Benefits and Strategies

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- eDCCO/Hybrid++ introduction
- DCCO and eDCCO advantages
- Electric-only driving and algorithms
- Vehicle platform and fuel economy projections
- DCCO transitions
- Vehicle drive cycle results
- Value proposition and summary

### **Tula Technology SAE Presentations**

- 2021-01-0459 Evaluation of a New High Efficiency Engine Concept with Atkinson cycle, Cooled EGR and Dynamic Skip Fire
- 2021-01-0450 Application of Dynamic Skip Fire for NOx and CO2 Emissions Reduction of Diesel Powertrains
- 2021-01-0446 Controls and Hardware Development of Multi-Level Miller Cycle Dynamic Skip Fire (mDSF) Technology
- 2020-01-0313 Fast Catalyst Light-Off with Dynamic Skip Fire
- 2019-01-1245 Instrumentation and Processor in Loop Verification for Dynamic Skip Fire Technology
- 2019-01-1054 Vibration Rating Prediction using Machine Learning in a Dynamic Skip Fire Engine
- 2019-01-0549 Dynamic Skip Fire Applied to a Diesel Engine for Improved Fuel Consumption and Emissions
- 2019-01-0227 mDSF: Improved Fuel Efficiency, Drivability and NVH Via DSF and Miller Cycle Synergies
- 2018-01-1162 Method to Compensate Fueling for Individual Firing Events in a 4-Cylinder Engine Operated with Dynamic Skip Fire
- 2018-01-1158 Machine Learning for Misfire Detection in a Dynamic Skip Fire Engine
- 2018-01-0891 λDSF: Dynamic Skip Fire with Homogeneous Lean Burn for Improved Fuel Consumption, Emissions and Drivability
- 2018-01-0864 Electrified Dynamic Skip Fire (eDSF) Design and Benefits
- 2016-01-0672 Fuel Economy Gains through Dynamic-Skip-Fire in Spark Ignition Engines
- 2015-01-1717 Modeling and Simulation of Airflow Dynamics in a Dynamic Skip Fire Engine
- 2015-01-0210 Misfire Detection in a Dynamic Skip Fire Engine
- 2014-01-1675 Methods of Evaluating and Mitigating NVH when Operating an Engine in DSF
- 2013-01-0359 Design and Benefits of Dynamic Skip Fire Strategies

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- All-at-once cylinder deactivation systems have lower cost and are attractive to customers
- DCCO extends coasting by eliminating retarding pumping torque encountered in typical DFCO, and prevents catalyst oxygenation
- Opportunity for electric driving with fully deactivated engine when torque demand is low
  - Electric driving doubles fuel cutoff time in WLTC
- Torque bump on exiting DCCO managed through use of MGU torque; more efficient than other methods





- Catalyst oxygen management: avoids air pumping through catalyst during decelerations, eliminates need for O2 purge with rich combustion
- Increased fuel off time: no entry delays, increased coasting time



# Synergy of DCCO with Mild Hybrid

- Increased regeneration by reducing pumping losses
- High value torque assist in using the energy through electric driving



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- Increased regeneration by reducing pumping losses
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### > Electric driving mode or ZEV mode

- Lengthens DCCO events with earlier entry and delayed exit
- During low torque maneuvers including coasting or mild decel leading to additional ZEV events

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- Engine stop in DCCO
  - Avoids return to idle and associated fueling
  - Increases inertia energy recuperation by eliminating pumping
- Engine start in DCCO
  - Improved first combustion after spin-up
  - Eliminates pumping losses during cranking  $\rightarrow$  reduced electrical energy required with better NVH
  - Eliminates air pumped into catalyst
- Reduced toxic emissions due to better catalyst management
- Reduced cold-start emissions due to better combustion after engine spin-up in deac

- Effectiveness of MGU torque assist quantified as fuel saved per unit electrical energy spent
- Most-effective torque assist with engine firing is near the maximum electrical system efficiency
- DCCO with electric driving is a higher-value use of battery energy than firing



# eDCCO Highly-Effective Use of Electrical Energy

- Below 95Nm flywheel torque request, ZEV driving has better TA effectiveness than firing the engine, especially at the lowest loads
- To limit the use of TA, a threshold of effectiveness is chosen, here 73 mg/kJ produces battery state of charge at the end of a drive cycle matching that at the beginning
- For I4+MH operation above 95Nm, TA improves engine efficiency only at the highest flywheel torque requests. A threshold of 60 mg/kJ maintains SoC
- The lower threshold indicates less opportunity to use battery energy in a highly-effective way



#### **ZEV** operation to replace low load ICE operation



- ZEV operation occurs at low torque where ICE operates inefficiently
- Operation spans a range of 4-8kW and 25Nm MGU tq
  - Depending on system efficiency and available battery energy

Base Vehicle	2016 Volkswagen Jetta SEL	
Test Weight	1588 kg	
Engine	EA888 1.8L gasoline	
	turbocharged direct injection	
Valvetrain	4 valves per cylinder, full-	
	authority deactivation,	
	operated in ganged mode	
Transmission	6-speed automatic with	
	torque converter clutch *	
Gear Ratios	4.459, 2.508, 1.556, 1.142,	
	0.851, 0.672	
Final Drive Ratio	3.23	
Driven Wheels	Front	
Tires	225/45 R17	

\* Torque converter clutch operated fully locked (no slip) in gears 3+ to emulate target vehicle application

#### Electrification

	Borg-Warner 12kW	
MGU	rated power permanent	
	magnet synchronous	
Inverter	Tula 550A power stage	
Battery	A123 8Ah 48V lithium	
	iron phosphate	
P0 Pulley	2.137	
Ratio		
FEAD	Litens bidirectional	
Tensioner		

• 40Nm MGU torque limit imposed

 With electric driving in DCCO strategy, no need for catalyst oxygen purge, and MGU managed DCCO exits, CO2 reduction of 5.1% is predicted over I4 mild-hybrid baseline



- Locked torque converter clutch introduces additional challenges for NVH
- Refiring of all cylinders at end of DCCO, at atmospheric manifold pressure, results in jarring engine torque not mediated by slipping TCC



 Brief DFCO period at the end of DCCO reduces manifold pressure and combustion torque on refiring



# **DCCO Exit and Entry – MGU Managed**

- Absorb excess torque on refiring using the MGU, energy captured in battery
- A combination of feedforward and feedback damping strategies shown effective



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- Under certain operating conditions such as low speeds, a ganged deactivation mechanism may still be capable of skip-firing
- This allows possibility of FD managed exits, and combination strategies



#### DCCO Exit with DFCO and Fire Density Ramping

### **Drive Cycle Results**



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Fuel Cut-off Time [s]	186	374
Catalyst O2 purge fuel [% of drive cycle fuel]	1.0	0
Electrical Regen Energy [MJ]	1.37	1.51
TA Effectiveness [mg/kJ]	61	90
Electrical TA Energy [MJ]	0.63	0.63
Battery SoC Change [%]	0	+6



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## **Catalyst Oxygen Management**



- During DCCO, no oxygen is introduced into the exhaust aftertreatment system
- On refiring the engine, significant catalyst management challenges are avoided
- No enriched air-fuel mixture to deoxygenate the catalyst
- Engine out CO and HC avoided, limiting reactants for NH<sub>3</sub> production
- Also inhibits NH<sub>3</sub> production by maintaining higher catalyst temperature by eliminating of air pumping











#### **Significant Toxic Emissions Reduction**



- WLTC CO and NOx reduced by 50% with respect to mild-hybrid I4 operation
- HC and CH4 reduced by 20 – 25%
- NH3 reduced by 80%
- Test vehicle achieved strictest proposed targets for Euro7 with margin
- Further reductions in emissions expected with implementation of deac in cold start and stop-start

- eDCCO can be mechanized with grouped deactivation valvetrain to minimize cost
- Controls and calibration well understood
- Favorable CO<sub>2</sub> and NVH results on 4-cylinder platform
- Favorable toxic emissions results, and further potential exists
- Estimated value proposition for 4-cyl at \$35/%CO<sub>2</sub> and 3-cyl at \$25/%CO<sub>2</sub>, against MH baseline
- High-value target applications of 3/4-cyl, P0/P1 48V mild hybrid

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